

Appendix D Example 15 – Diagonal Bracing of Single Tier Framed Bent – Bolted Connections

Refer to *Falsework Manual*, Section 6-3, *Diagonal Bracing* and Section 5-3, *Timber Fasteners*. This example demonstrates how to determine if the bracing system of a single tier framed bent is adequate. All connections are bolted.

Given Information



Figure D-15-1. Single Tier Framed Bent with Multiple Diagonal Bracing

2% Dead Load = 4200 lb Wind Load = 4100 lb

Posts:

12 x 12 Rough Douglas Fir-Larch #1 (G=0.50)

Diagonal Braces: 2x8 Douglas Fir-Larch #2 (G=0.50)

Connectors: End of brace to post: ³/₄ " Ø Bolt Center of brace to post: ³/₄ " Ø Bolt (All bolts in single shear)

Determine if the Bracing System is Adequate

1. Determine the strength of the bolted connection between brace and post:

(See Example Problem #10 for additional information)

Adjusted connection capacity (Z') = 1530 lb

2. Determine strength of diagonal braces in tension:

Reference design value in tension $F_t = 575 \text{ psi}$ (NDS supplement table 4A)

Adjustment factors from NDS table 4.3.1:

C _D = 1.25	Duration Factor for 2% lateral loading
См = 1.0	<i>Wet Service Factor NDS table 4A (Assume < 19% moisture content)</i>
C _t = 1.0	Temperature Factor NDS table 2.3.3 (Temp up to 100°F)
C _F = 1.2	Size Factor NDS Table 4A
Ci = 1.0	Incising Factor NDS 4.3.8

Adjusted design value Ft' = Ft (CD)(CM)(Ct)(CF)(Ci) = 863 psi

Tension capacity = 863 psi (1.5")(7.25") = 9385 lb

3. Determine strength value of the tension members:

9385 lb > 1530 lb :: Connection controls tension

4. Calculate the horizontal component of the strength value for tension members:





5. Determine the capacity of diagonal brace in compression:

Determine connection capacity of diagonal brace in compression:

Connection capacity = 1530 lb (from step 1 above.)

Determine the capacity of diagonal brace in compression:

Reference design value in compression $F_c = 1350$ psi (NDS supplement table 4A)

Adjustment factors from NDS table 4.3.1:

Duration Factor for 2% lateral loading
Wet Service Factor NDS table 4A (Assume < 19% moisture content)
Temperature Factor NDS table 2.3.3 (Temp up to 100°F)
Size Factor NDS Table 4A
Incising Factor NDS 4.3.8
Column Stability Factor NDS 3.7.1 (unsupported length = $\frac{14.14}{2}$ = 7 07')

Adjusted design compression value F_c ' = $F_c (C_D)(C_M)(C_t)(C_F)(C_i)(C_P)$ = 147 psi

Compression brace capacity = 147 psi(1.5")(7.25") = 1599 lb

6. Determine the strength value of the compression members

1599 lb > 1530 lb ∴ connection controls compression

Limit to ½ theoretical strength for compression values: See section 6-3.02 *Wood Cross Bracing.*

Reduced compression brace capacity = $\frac{1530 \text{ lb}}{2}$ = 765 lb

7. Calculate the horizontal component of the strength value for the compression member





8. Calculate the total resisting capacity of the diagonal bracing system:

Summarize Result for 2% Dead Load



Figure D-15-4. Total Resisting Capacity for 2% Dead Load

Total resisting capacity = $\Sigma(C + T) = 541 + 1082 + 541 + 1082 = 3246$ lb

Resisting capacity = 3246 lb < Horizontal demand force = 4200 lb

Bracing system is inadequate for 2% Dead Load

Summarize Result for Wind Load

Repeat above process for wind load to calculate the Resisting Capacity, using $C_D = 1.6$ rather than 1.25. All other factors are the same.



Figure D-15-5. Total Resisting Capacity for Wind Load

The Resisting Capacity for wind load can also be derived by multiplying the resisting

capacity for 2% Dead Load (above table) by the ratio $\frac{C_D \text{ wind}}{C_D 2\%} = \frac{1.6}{1.25}$

Resisting Capacity = 3246 lb $\left(\frac{1.6}{1.25}\right)$ = 4155 lb > Horizontal Demand Force = 4100 lb

Bracing system is adequate for Wind Load

Bracing system does not have enough capacity to resist <u>both</u> 2% Dead Load and Wind Load.

Bracing system is inadequate.